

## Chapter 4 Summary

### System Response

high fidelity measurement system requirements:

1. Amplitude linearity
2. Adequate bandwidth
3. Phase linearity

*amplitude linearity:*  $V_{\text{out}}(t) - V_{\text{out}}(0) = \alpha[V_{\text{in}}(t) - V_{\text{in}}(0)]$

*Fourier series:*  $F(t) = C_0 + \sum_{n=1}^{\infty} A_n \cos(n\omega_0 t) + \sum_{n=1}^{\infty} B_n \sin(n\omega_0 t)$

*Fourier coefficients:*

$$A_n = \frac{2}{T} \int_0^T F(t) \cos(n\omega_0 t) dt$$

$$B_n = \frac{2}{T} \int_0^T F(t) \sin(n\omega_0 t) dt$$

$$C_0 = \frac{1}{T} \int_0^T F(t) dt = \frac{A_0}{2}$$

*decibel:*  $\text{dB} = 20 \log_{10} \left( \frac{A_{\text{out}}}{A_{\text{in}}} \right)$

**frequency response curve:** plot of the **amplitude ratio**,  $A_{\text{out}}/A_{\text{in}}$ , vs. the input frequency

**bandwidth:** the range of frequencies a system can adequately reproduce.

*cutoff frequency points:*  $\frac{A_{\text{out}}}{A_{\text{in}}} = \sqrt{\frac{P_{\text{out}}}{P_{\text{in}}}} = \sqrt{\frac{1}{2}} \approx 0.707$

*phase linearity:*  $f = k \cdot f$

zero order system:

$$A_0 X_{\text{out}} = B_0 X_{\text{in}}$$
$$X_{\text{out}} = \frac{B_0}{A_0} X_{\text{in}} = K X_{\text{in}}$$

first order system:

$$\tau \frac{dX_{\text{out}}}{dt} + X_{\text{out}} = KX_{\text{in}}$$
$$X_{\text{out}}(t) = KA_{\text{in}}(1 - e^{-t/\tau})$$

second order system:

$$m \frac{d^2x}{dt^2} + b \frac{dx}{dt} + kx = F_{\text{ext}}(t)$$

undamped ( $b = 0$ ):  $x_h(t) = A \cos\left(\sqrt{\frac{k}{m}} t\right) + B \sin\left(\sqrt{\frac{k}{m}} t\right)$

natural frequency:  $\omega_n = \sqrt{\frac{k}{m}}$

critically damped ( $b = b_c$ ):  $x_h(t) = (A + Bt)e^{-\omega_n t}$

critical damping constant:  $b_c = 2\sqrt{km} = 2m\omega_n$

damping ratio:  $\zeta = \frac{b}{b_c} = \frac{b}{2\sqrt{km}}$

underdamped ( $\zeta < 1$ ):

$$x_h(t) = e^{-\zeta\omega_n t} [A \cos(\omega_n \sqrt{1 - \zeta^2} t) + B \sin(\omega_n \sqrt{1 - \zeta^2} t)]$$

damped natural frequency:  $\omega_d = \omega_n \sqrt{1 - \zeta^2}$

overdamped ( $\zeta > 1$ ):

$$x_h(t) = A e^{(-\zeta + \sqrt{\zeta^2 - 1})\omega_n t} + B e^{(-\zeta - \sqrt{\zeta^2 - 1})\omega_n t}$$

frequency response analysis:

input:  $x_{\text{in}}(t) = A_{\text{in}} \sin(\omega t)$

output:  $x_{\text{out}}(t) = A_{\text{out}} \sin(\omega t + \phi)$

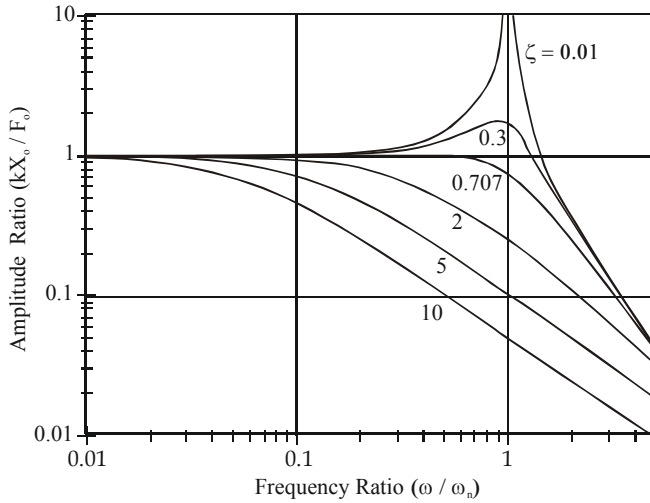
transfer function:  $G(s) = \frac{X_{\text{out}}(s)}{X_{\text{in}}(s)}$

amplitude ratio:  $\frac{A_{\text{out}}}{A_{\text{in}}} = \text{mag}(G(j\omega)) = \|G(j\omega)\|$

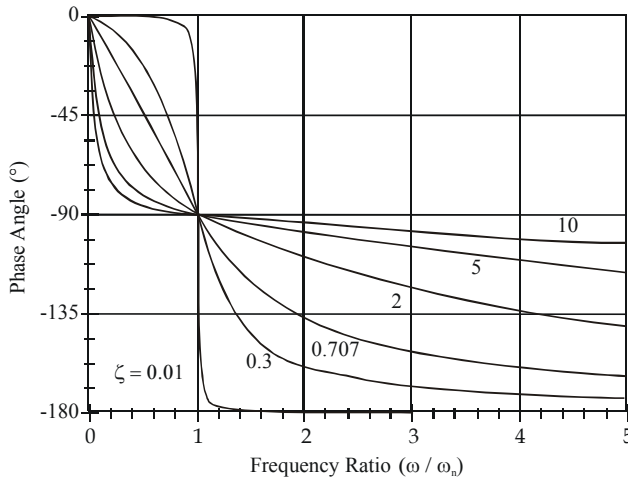
phase angle:  $\phi = \arg(G(j\omega)) = \angle G(j\omega)$

second order system frequency response:

amplitude ratio: 
$$\frac{X_o}{F_o/k} = \frac{1}{\left[ 1 - \left( \frac{\omega}{\omega_n} \right)^2 \right]^2 + 4\zeta^2 \left( \frac{\omega}{\omega_n} \right)^2 \right]^{1/2}}$$



phase angle: 
$$\phi = -\tan^{-1} \left\{ \frac{2\zeta}{\frac{\omega_n}{\omega} - \frac{\omega}{\omega_n}} \right\}$$



modeling analogies:

Generic quantity	Mechanical translation	Mechanical rotation	Electrical	Hydraulic
Effort ( $E$ )	Force ( $F$ )	Torque ( $T$ )	Voltage ( $V$ )	Pressure ( $P$ )
Flow ( $F$ )	Speed ( $v$ )	Angular speed ( $\omega$ )	Current ( $i$ )	Volumetric flow rate ( $Q$ )
Displacement ( $q$ )	Displacement ( $x$ )	Angular displacement ( $\theta$ )	Charge ( $q$ )	Volume ( $V$ )
Momentum ( $p$ )	Linear momentum ( $p = mv$ )	Angular momentum ( $h = J\omega$ )	Flux linkage ( $I = N\Phi = Li$ )	Momentum/area ( $\Gamma = IQ$ )
Resistor ( $R$ )	Damper ( $b$ )	Rotary damper ( $B$ )	Resistor ( $R$ )	Resistor ( $R$ )
Capacitor ( $C$ )	Spring ( $1/k$ )	Torsion spring ( $1/k$ )	Capacitor ( $C$ )	Tank ( $C$ )
Inertia ( $J$ )	Mass ( $m$ )	Moment of inertia ( $J$ )	Inductor ( $L$ )	Inertance ( $J$ )
Inertia energy storage (special case)	$F = \dot{p}$ ( $F = ma$ )	$T = \dot{h}$ ( $T = J\alpha$ )	$V = \dot{\lambda}$ ( $V = L di/dt$ )	$P = \Gamma$ ( $P = I dQ/dt$ )
Capacitor energy storage	$F = kx$	$T = k\theta$	$V = (1/C)q$	$P = (1/C)V$
Dissipative	$F = bv$	$T = B\omega$	$V = Ri$	$P = RQ$